# **Intrinsic Viscosity Calculated by Computer**

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### **Synopsis**

A computer program has been devised for routine use which processes raw data such as polymer sample weight, moisture content, solution volume, and viscometer flow times to calculate a least-squares-derived intrinsic viscosity. In addition to eliminating errors inherent in graphic solutions and freeing technicians from tedious calculation, the computer output provides the 95% confidence interval of the intrinsic viscosity.

## INTRODUCTION

The well-known calculations required in determining intrinsic viscosities of polysaccharides and other polymers are tedious and subject to human error in curve fitting. Usually, intrinsic viscosity is determined by a graphic solution in which the value of reduced viscosity is extrapolated to zero concentration on a reduced viscosity-concentration plot. Furthermore, the graphic solution does not facilitate statistical treatment of precision. Precision of an intrinsic viscosity is important in determining real effects of physical and chemical treatments on polymer molecular weight or structure as inferred from viscosity changes.

To obviate these difficulties, a computer program was prepared for rapidly calculating intrinsic viscosity from such raw data as grams of polymer, polymer moisture, dilution volume, and viscometer flow times of solvent and solutions. The essential features of computer processing intrinsic viscosity data are:

1. A raw data Intrinsic Viscosity Input Form (Fig. 1) that is completed by the technician in the laboratory and from which data cards are keypunched.

2. Output from computer (Fig. 2) that includes: (a) a one-line, 80character description of sample, solvents, operator, and date; (b) raw data printout; (c) summary of reduced viscosity (Nsp/C) and corresponding concentration (C); (d) intrinsic viscosity to three decimal places; (e) 95% confidence interval (C.I.) of intrinsic viscosity value.

3. A graphic representation (Fig. 3) of the data points to enable ready identification of any outliers. This optional feature requires some additional programming (not described here) and a computer-plotter attachment. However, as an alternative to the plotter, whenever the C.I. ex-





### INTRINSIC VISCOSITY

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COMMERCIAL AMYLOPECTIN (9517-28) . VISCOMETER A21. OMSO SULVENT. 11-16-71. 8.T.H. GRAMS SAMPLE 0.0904 VOLUMETRIC 50.0 ML MOISTURE 6.82 PERCENT FLOW TIMES. SEC. AVERAGE DATA SOLVENT 166-6 166-6 166-6 SOLN C1 199-5 199-5 199-5 SOLN C2 181-9 182-0 181-9 181-9 166.6 199.5 181.9 SOLN C3 176+6 176+6 176+8 SOLN C4 173+9 174+1 174+1 176.6 1/6./ 174.0 SUMMARY DILN VISCOSITY REL SPECIFIC REDUCED CONC .PCT 0.1648 1.0 1.1974 0.1974 1.1979 0.0824 2.0 1.0919 0.0919 1+1159 0.0549 9.0604 1.1005 3.3 .0634 4.0 0.0412 1.0446 J-0445 1.0825 INTRINSIC VISCOSITY= 1.045 DL/GRAM C I = 0.021 Fig. 2. Computer output from intrinsic viscosity program.

ceeds an established norm, Nsp/C versus C should be plotted from values calculated in the computer output (Fig. 2). In this manner any disproportionate error contributed by a single data point set can be determined.

Outputs can be bound to give a permanent laboratory notebook record of raw and derived data.

### **PROGRAM OPERATION**

The mechanics of the program use are illustrated by the example data in Figure 1:

1. Preparation of Intrinsic Viscosity Input Form (Fig. 1).

Card 1:

Column 1. Total number of polymer dilutions to be run.

Column 2. Code number indicating whether or not a different viscometer is used for each polymer concentration.

Columns 3-8. Weight in grams, "as is," of polymer.



Fig. 3. Plotter output showing scatter of experimental points and least-squares-derived straight line.

Columns 9-13. Volume, in milliliters, to which the polymer is diluted in the stock solution  $(C_1)$ .

Columns 14–18. Per cent moisture content of polymer.

However, if one begins with a polymer solution of known concentration, columns 3-18 (Card 1) may be filled assuming a a 100-ml volume and zero moisture.

Card 2:

Columns 1–80. All references and comments.

Card 3:

Columns 1-50 (by groups of five). Solvent flow times, to the nearest tenth second. If an average value for the viscometer is already known, it should be recorded in columns 1-5.

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// JOB
// FOR
. ONE WORD INTEGERS
· EXTENDED PRECISION
• IOGS { CARD + 1132 PRINTER }
DIMENSION FLOWS(10)+FLOW(10)+DIFLN(9)+RLVIS(9)+SPVIS(9)
       DIMENSION X(9)+Y(9)+ST(7)
DIMENSION IOUTC(80)
      DATA $1(7),$1(4),$1(5),$1(4),$1(3),$1(2),$1(1)
1/ 2.3646,2.4469,2.5706,2.7764,3.1825,4.3027,12.706 /
  200 READ(2+205)NOSLN+NOSET+GRSOL+VOLML+PCTM
  205 FORMAT(211+F6+4+F5+2+F5+3)
       IF(NOSLN)295+295+210
  295 CALL EXIT
210 ACONC=(GRSOL-PCTM+GRSOL/100.1+100./VOLML
       WRITE(3+208)
  208 FORMAT( 1120X INTRINSIC VISCOSITY')
  READ (2+222) IOUTC
222 FORMAT (80A1)
       WRITE(3+223)IOUTC
  223 FORMAT( '0'80A1)
       WRITE(3+212)GRSOL+VOLML+PCTM
  212 FORMAT('O GRAMS SAMPLE'F8.4." VOLUMETRIC'F6.1." ML MOISTU
1F6.2' PERCENT'/'O FLOW TIMES. SEC.'/'O AVERAGE'11X'DATA')
                                                                          MOISTURE!
       DO 250 J=1.NOSLN
IF(NOSET)214.211.214
  211 IF(J-1)227+214+227
  214 READ(2+215)FLOWS
  215 FORMAT(10F5+1)
       NO=0
       TFLOS=0.
       DO 220 1=1+10
IF(FLOWS(1))220+220+218
  218 NO=NO+1
       TFLOS=TFLOS+FLOWS(1)
  220 CONTINUE
       TFLOS=TFLOS/NO
       WRITE(3,225)TFLOS,(FLOWS(1),I=1,NO)
  225 FORMAT(3XF6+1+4X'SOLVENT*10F6+1)
  227 READ(2+232)DIFLN(J)+FLOW
  232 FORMAT(F5.2.10F5.1)
       NO=0
       TFLO=0.
       DO 240 I=1+10
IF(FLOW(1))240+240+235
  235 NO=NO+1
       TFLO=TFLO+FLOW(1)
  240 CONTINUE
       TFLO=TFLO/NO
       WRITE(3+230)TFLO+J+(FLOW(1)+1=1+NO)
  230 FORMAT(3XF6.1.4X'SOLN C'11.10F6.1)
                                 Fig. 4 (continued)
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```
X(J)=ACONC/DIFLN(J)
        RLVIS(J)=TFLO/TFLOS
        SPVIS(J)=RLVIS(J)=1.
        Y(J)=SPV15(J)/X(J)
  250 CONTINUE
  WRITE(3+255)
255 FORMAT ('OSUMMARY'/
  255 FORMAT ('OSUMMARY'/ 14X'DILN'8X'VISCOSITY'
1/3X'CONC+PCT FACTOR REL SPECIFIC REDUCED'/1X)
WRITE(3+245)(X(J)+DIFLN(J)+RLVIS(J)+SPVIS(J)+Y(J)+J=1+NOSLN)
245 FORMAT (1XF9+4+F8+1+F10+4+F8+4+F9+4)
        N=NOSLN
        IF(N-1)200+200+3
     3 EN=N
        $1GX=0.0
        $16Y=0.0
        SIGXX=0.0
        SIGXY=0.0
       DO 101 1=1+N
$IGX=$IGX+X(1)
        $1GY=$1GY+Y(1)
$1GXX=$1GXX+X(1)*X(1)
        $1GXY=$1GXY+X(1)=Y(1)
  101 CONTINUE
        A=($IGY+SIGXX-SIGX+SIGXY)/(EN+SIGXX-SIGX++2)
        B=(EN+SIGXY-SIGX+SIGY)/(EN+SIGXX-SIGX++2)
        ERA=0.
DO 70 I=1.N
YEA=X(I)+B+A
        YERA=Y(1)-YEA
        ERA=ERA+YERA#YERA
    TO CONTINUE
        DF=NDF
        1F(NDF)340+340+342
  340 CI=0.
        GO TO 348
  342 CI=SURT(ERA/DE+(1./EN+SIGX++2/(EN++2+SIGXX-EN+SIGX++2)))
   CI-CI+ST(NDF)
348 WRITE(3+260)A+CI
   260 FORMAT ('O
                       INTRINSIC VISCOSITY='F8.3' DL/GRAM'5X'C I ='F6.3)
        GO TO 200
        END
// XEQ
    0904 50
40
                  882
COMMERCIAL AMVLOPECTIN (9517-28), VISCOMETER A21, DMSO SOLVENT, 11-16-71, B.T.M.
1666 1666 1666
1 1995 1995 1995
        1819 1820 1819
1766 1766 1768
  2
                            1819
                           1767
        1739 1741 1741
٥
```



Card 4:

Columns 1-5. Dilution factor; e.g., a dilution factor of the stock solution is 1.0 and a 1:1 dilution of the stock solution is a dilution factor of 2.

Columns 6–55 (by groups of five).  $C_1$  flow time (initial concentration).

At this point, if only one viscometer is used throughout as in the sample data (Fig. 1), there will be only one solvent flow time card. However, when there is a different viscometer for each polymer concentration, the solvent flow time card is paired with the corresponding solution flow time card according to the card sequence shown in Figure 1. Any number of polymer solutions up to a total of nine may be run with the present program.

2. Data cards keypunched from the Intrinsic Viscosity Input Form, placed in the order shown in Figure 1, follow the program cards in the computer processing.

### CALCULATIONS

The program computes from experimental data, by the method of least squares, the slope and intercept of eq. (1):

$$X = (M) (C) + \eta \tag{1}$$

where X = Nsp/C, M = slope, C = concentration, g/100 ml; and  $\eta = \text{Intercept}$  (intrinsic viscosity), dl/g.

Presumably, regression of reduced viscosity on polymer concentration is linear. Although our Fortran program would be inadequate for nonswamped polyelectrolytes, it could be modified to process quadratic regression and, thereby, extrapolate reduced viscosity more accurately to infinite dilution.

C.I. is at the 95% level and is defined by eq. (2):

C.I. = 
$$t_{\alpha,N-2} \cdot S_{Y \cdot X} \sqrt{\frac{1}{N} + \frac{\bar{X}^2}{\Sigma (X_i - \bar{X})^2}}$$
 (2)

where  $S_{Y,X}$  = standard error of estimate of the regression of reduced viscosity on concentration;  $t_{\alpha,N-2}$  = statistical "t" evaluated for N-2 degrees of freedom where  $\alpha$  is the probability of a larger value of t (sign ignored) and  $100(1-\alpha)$  is the level of confidence; N = number of experimental points;  $\overline{X}$  = average value of reduced viscosity; and  $X_i$  = values of *i* numbers of reduced viscosity.

The meaning of C.I. at the 95% level is: The true or population intrinsic viscosity will be included within the confidence limits of 95% of the viscosity determinations. It is important to know that the *t* value in eq. (2) has values for N = 3, 4, 5, and 6 observations of  $t_{\alpha,N-2} = 12.71$ , 4.30, 3.18, and 2.78, respectively. Consequently, C.I. is reduced about one third in going from three to four points because two degrees of freedom are lost in the regression, which for three observations leaves only one degree of freedom.

The computer program, which is in Fortran IV, is given in Figure 4.

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